

AFCRL-66-586

"Implementation and Performance of the Maximum-Likelihood Detector  
in a Channel with Intersymbol Interference"

by

Robert A. Gonsalves



Northeastern University  
360 Huntington Avenue  
Boston, Massachusetts

Contract No. AF19(628)-3312

Project No. 4610

Task No. 461003

Scientific Report No. 5

August 1966

Charles F. Hobbs, CRBK

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AIR FORCE CAMBRIDGE RESEARCH LABORATORIES  
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Arthur A. Giordano helped to establish the second piece-wise linear approximation of Section III and Eric Reid programmed Equation (28) to provide the graphs of Figures 6 through 9.

## ABSTRACT

It is shown that the maximum-likelihood (ML) detector for noisy, binary channel with restricted intersymbol interference (ISI) consists of a matched filter followed by a tapped delay line. The useful output is a nonlinear function of the tap outputs. Bounds on the per-symbol probability of error indicate that a gross approximation to the ML detector performs as well as an optimum linear detector. The major assumptions are (1) bi-polar binary signals, (2) ISI only between adjacent bauds, (3) stationary additive white, Gaussian noise, and (4) perfect synchronization. Extensions are suggested to remove assumptions (1) and (2) and to handle stationary, non-white Gaussian noise.

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## 1. Introduction

In a previous report<sup>1</sup> it was shown that the maximum-likelihood (ML) detector for a noisy, binary channel with memory could be implemented using two matched filters, one delay element and a recorder-play-back system. In this report we will modify and streamline the detector structure so that it includes only one matched filter and so that decisions can be made sequentially, in real time. We find new upper and lower bounds for the detector's performance by certain limiting techniques. We also discuss some extensions to the earlier work.

There are four key assumptions for the main body of this report:

- (1) The signal is

$$\sum_{k=-\infty}^{\infty} \mu_k s(t-kT),$$

where  $\mu_k = +1$  or  $-1$ , represents the  $k^{\text{th}}$  symbol to be transmitted. The  $\mu_k$ 's are independent and  $s(t)$  is known exactly. Thus we focus our attention on the binary detection of a known signal. In Section 5 we discuss briefly the multi-level case. If  $s(t)$  is not known exactly, then we assume that it can be suitably measured during a brief calibration run or can be determined, adaptively, during transmission.

- (2) The signal  $s(t)$  is smeared only into one adjacent baud. Thus  $s(t)$  lasts only from 0 to  $2T$ . This restriction is also examined in Section 5.

- (3) The noise is white, additive and Gaussian.

Colored noise can be handled by suitable pre-whitening<sup>2</sup> prior to detection. In that case  $s(t)$  would be the output of the pre-whitening filter and would be subject to restriction

(2) on page 1.

- (4) Synchronism is maintained between transmitter and receiver. This may be achieved, for example, by the transmission of recurrent synch pulses.

The ML detector discussed in this report is new in two respects. First of all, although it has the general appearance of the linear, tapped-delay line detectors offered by Lucky<sup>3</sup> and by others<sup>4,5</sup>, it has been developed without the constraint of linearity. Thus the ML detector will always yield a probability of error that is smaller than the corresponding linear detector (except in some limiting cases where the performances will be identical). In this sense the ML detector is mathematically equivalent to that derived in the earlier report<sup>1</sup>, the implementation is different and is, in fact, inspired by the linear detectors of Lucky<sup>3</sup> and Tufts.<sup>5</sup>

Finally, the new detector structure suggests a piece-wise linear approximation to the optimum detector, which is quite simple to implement. The approximation is an extension to the class of "feedback tail cancellation" schemes discussed by Tufts and others (see Tufts<sup>5</sup> and the "switched mode" detector of Aein and Hancock<sup>6</sup>). Because of its simplicity and near optimum performance, it merits consideration in an actual binary transmission system.



## 2. The Detector Specification and Structure

In [1] we show that the ML detector first computes

$$A_k = \frac{4}{N_0} \int_{kT}^{(k+2)T} y(t) s(t-kT) dt, \quad (1)$$

where  $y(t)$  is the received signal,

$$y(t) = \sum_{k=-\infty}^{\infty} \mu_k s(t-kT) + n(t), \quad (2)$$

and  $n(t)$  is the additive, white, Gaussian noise of double-sided power spectral density  $N_0/2$  watts per cps.  $A_k$  represents the correlation of the signal  $(+)s(t-kT)$  with the received signal and can be implemented with a matched filter or with a multiplier and integrator.

The detector then bases its decision about the polarity of  $\mu_k$  on the statistic  $\Lambda_k$  <sup>1</sup>,

$$\begin{aligned} \Lambda_k = & A_k + Z\{A_{k-1} + Z\{A_{k-2} + \dots\}\} \\ & + Z\{A_{k+1} + Z\{A_{k+2} + \dots\}\}, \end{aligned} \quad (3)$$

where

$$Z\{x\} = \log_e \frac{e^x + e^R}{1 + e^{x+R}} \quad (4)$$

and

$$R = \frac{4}{N_0} \int_0^{2T} s(t) s(t+T) dt. \quad (5)$$

For example, if the source probabilities are equal and the costs associated with each type of error are equal, then the detector decides

$$\mu_k = \begin{cases} 1 & \text{if } \Lambda_k > 0 \\ -1 & \text{if } \Lambda_k < 0 \end{cases}.$$

Note that we may express R as

$$R = 2\rho r \quad (6)$$

where  $\rho$ , defined as

$$\rho = \frac{\int_0^{2T} s^2(t) dt}{\frac{N_0}{2}}, \quad (7)$$

is the signal-to-noise ratio and  $r$ , defined as

$$r = \frac{\int_0^{2T} s(t) s(t+T) dt}{\int_0^{2T} s^2(t) dt}, \quad (8)$$

will be called the index of interference and is a measure of the harmful effects of intersymbol interference. Now  $r$  is loosely bounded by

$$-1 < r < 1$$

so we expect that in the face of severe interference  $R$  will have values of the same order of magnitude as  $\rho$ .

Equations (2) and (3) define the ML detector and the corresponding structure is shown in Fig. 1. Note the similarity between this structure and those of Lucky<sup>3</sup> and of Tufts<sup>4</sup>, that is, a matched filter followed by a tapped delay line. In this structure, however, the useful output is not merely a weighted sum of the tap outputs. Here each output is added to its neighbor after that neighbor is passed through a non-linear amplifier (the box labelled Z and defined by Equation (4)). The M taps to the left of the center tap, the useful output, indicate that M bauds of the past data have been optimally processed to aid in the decision on  $\mu_k$ . The N taps to the right indicate that N future bauds have also been considered. In theory one should let  $M \rightarrow \infty$  and  $N \rightarrow \infty$  to achieve the optimum detector structure. We can, in fact, achieve  $M \rightarrow \infty$ , that is, we can consider all past data, by a modification of Fig. 1. This modification is shown in Fig. 2. Obviously, a consideration of all future data required infinite delay (for an infinite binary sequence) so a finite N must be chosen based on a study of cost per additional section versus improved performance per additional section (assuming the associated increased delay is acceptable). Such a study is very difficult analytically and is probably best done experimentally.

One of the interesting features of the detector structure of Fig. 2 is that all the non-linear amplifiers, the Z boxes, are identical. Therefore, knowing the signal shape  $s(t)$  (so that the matched filter can be constructed), the detector structure is determined by a specification of the parameter R as given by (5) or (6), since the amplifier characteristics depend only on R. In Fig. 3 we show the Z-box amplifier input-output characteristics for several typical values of R. Note that these curves are fairly well behaved and saturate at  $\pm R$ .

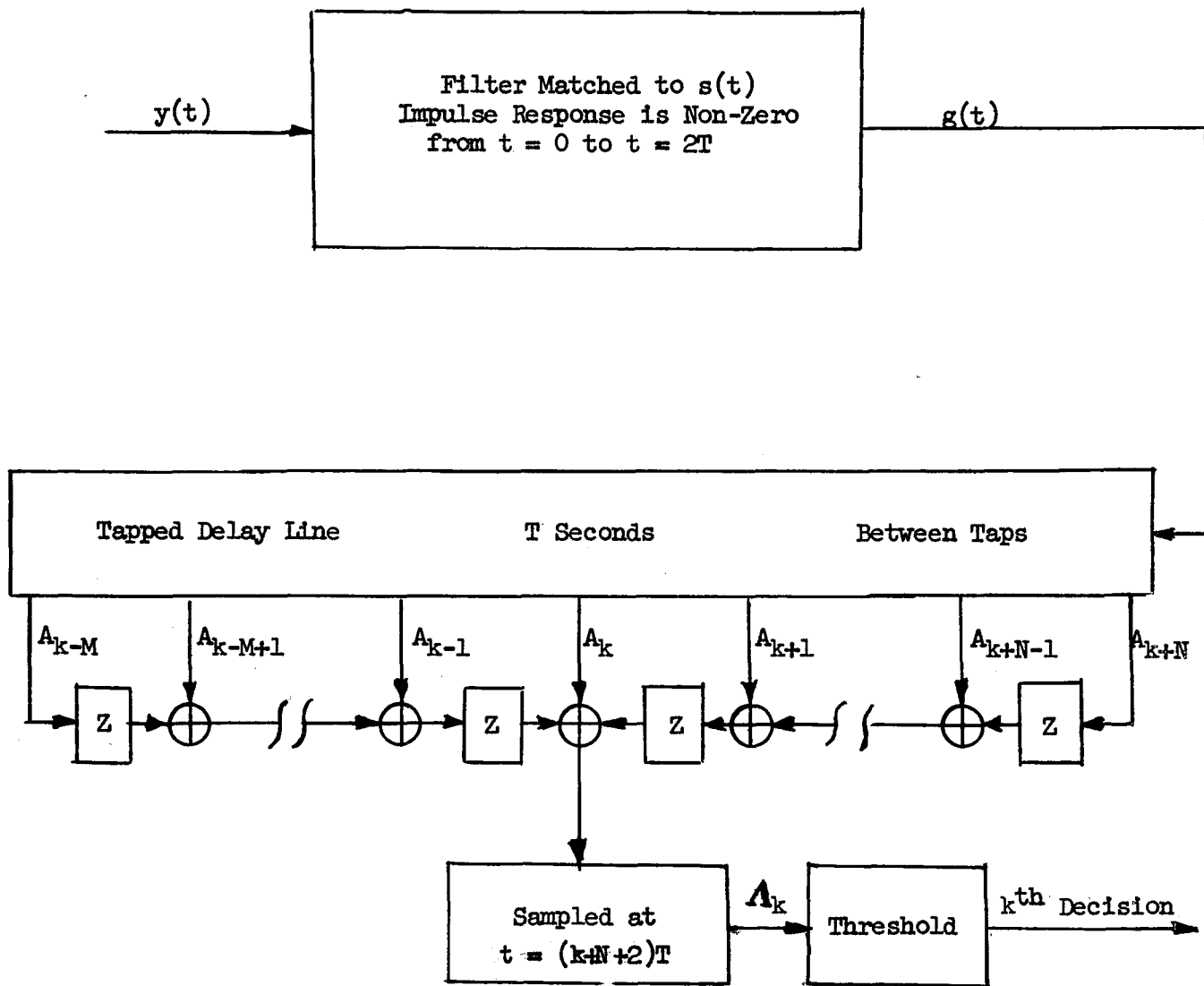


Fig. 1 The ML Receiver

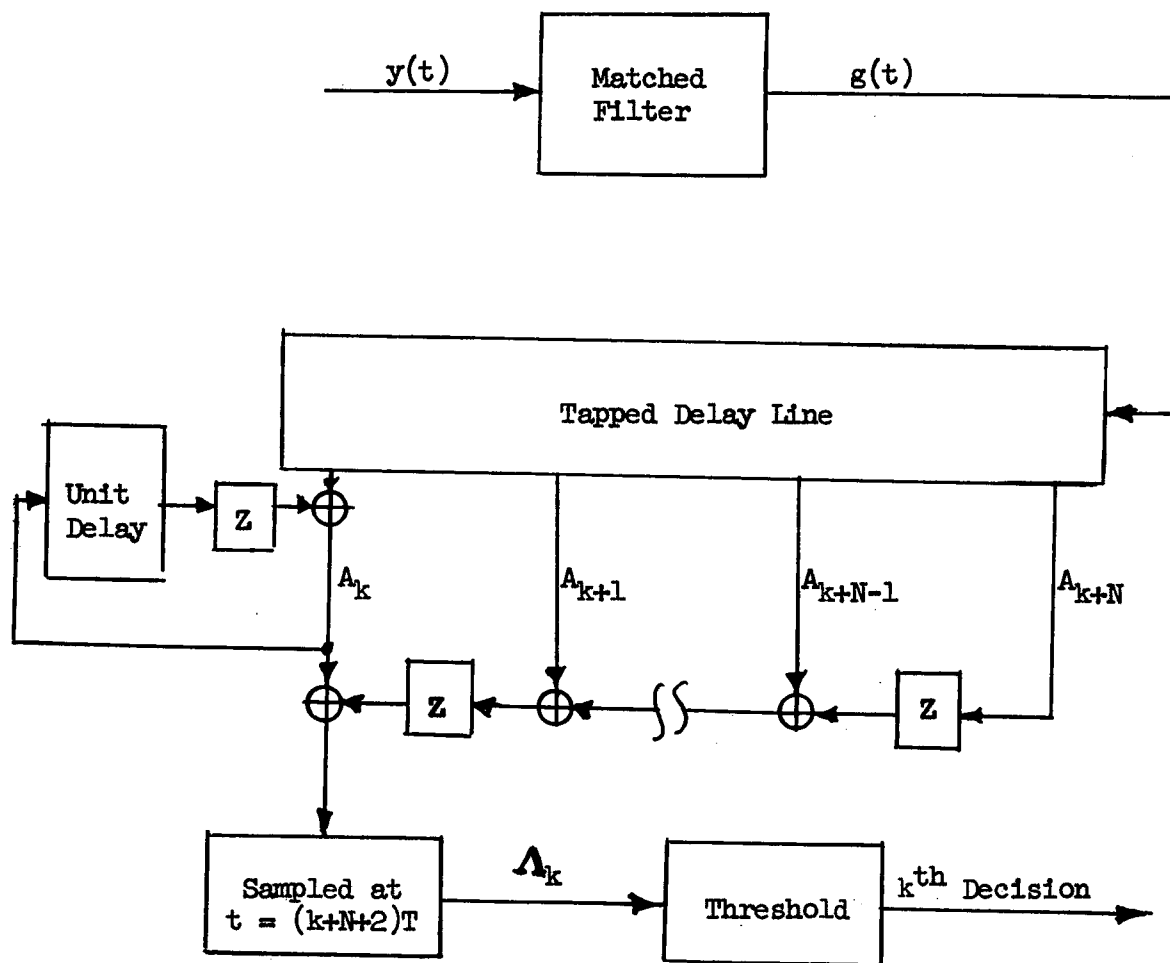


Fig. 2 A Simplified ML Receiver

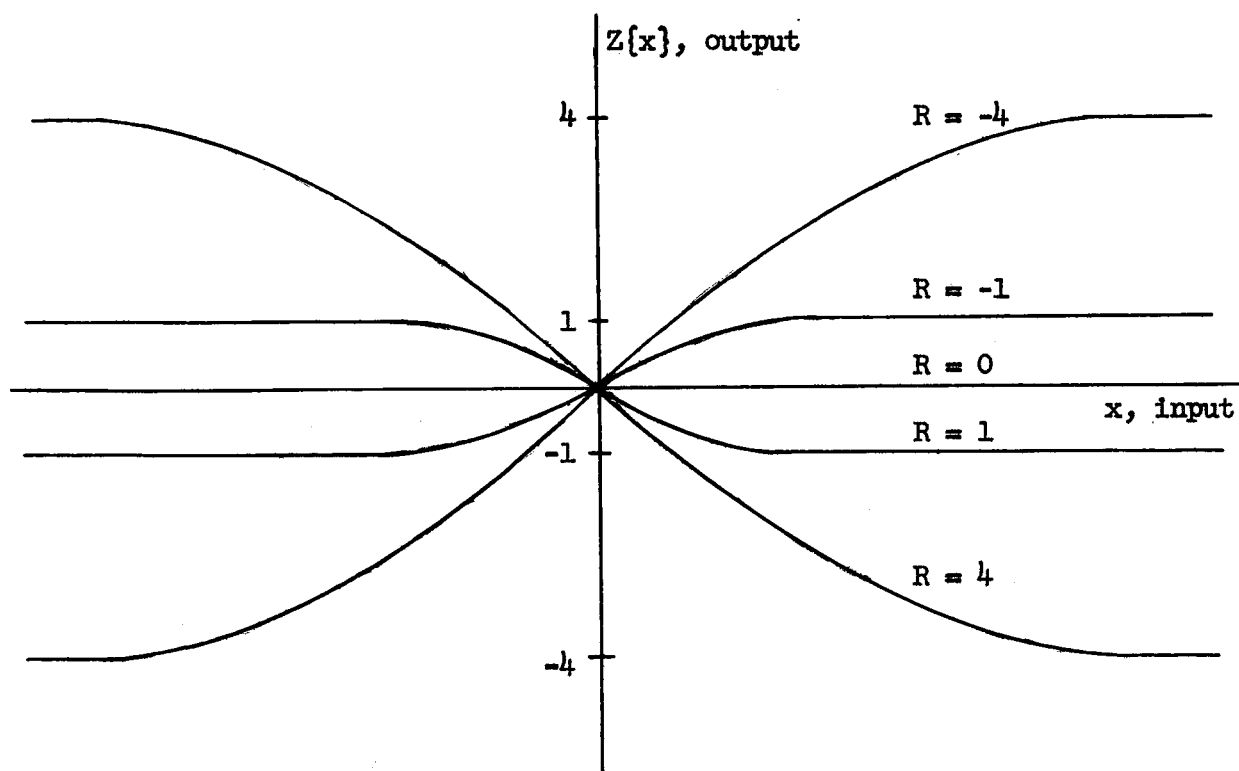


Fig. 3 The Non-Linear Amplifier,  $Z\{x\}$

To provide insight into the detector operation let us assume that the detector of Fig. 2 uses no tapped delay line at all. Hence

$$\Lambda_k = A_k + Z\{A_{k-1} + Z\{A_{k+2} + \dots\}\}.$$

We see that the  $k^{\text{th}}$  decision statistic contains first of all the correlation of  $s(t-kT)$  with the received signal, namely  $A_k$ . The other additive term is bounded by  $\pm R$ . In fact, assuming high SNR,  $A_{k-1}$  will be either large positive for  $\mu_{k-1} = 1$  or large negative for  $\mu_{k-1} = -1$ . Thus referring to Fig. 3, we will subtract  $R$  from  $A_k$  if  $\mu_{k-1}$  is positive and we will add  $R$  to  $A_k$  if  $\mu_{k-1}$  is negative. This addition or subtraction of  $R$  is mathematically equivalent to subtracting out the channel memory and is, therefore, a "feedback tail cancellation" scheme as mentioned in the introduction. The novelty here is that the tail cancellation occurs on a probabilistic basis. That is, we do not simply allow  $R$  or  $-R$  but we choose an intermediate value based on  $A_{k-1} + Z\{A_{k-2} + \dots\}$ , which is a measure of our certainty concerning  $\mu_{k-1}$ .

To examine the effect of the future data on the detector, we may consider that the data has been received with time reversed. Thus the "tail" of the original pulse becomes the main body of the new pulse and vice-versa. We can perform a similar, probabilistic tail cancellation. One then combines the information concerning past and future in the center tap to obtain the ML statistic.

### 3. Piece-Wise Linear Approximations

Two, successively better approximations to the ML detector are considered. Both are really approximations on the function  $Z\{x\}$  so that the block diagram specification of Fig. 2 is still applicable.

The first approximation is  $Z'\{x\}$ ,

$$Z'\{x\} = -R \operatorname{Sgn}\{x\} \quad (9)$$

where

$$\operatorname{Sgn}\{x\} = \begin{cases} 1, & x > 0 \\ -1, & x < 0. \end{cases}$$

If one considers only past data, then the resulting detector is exactly a tail cancellation scheme as previously discussed. Consideration of future data, as is done in Fig. 2, represents an improvement over previous detectors of this type. The performance of this detector, with a slight modification, is considered in the next section and serves as the upper bound on the ML detector.

A good approximation  $Z''\{x\}$  to  $Z\{x\}$  is shown in Fig. 4. In that figure the attenuator,  $A$ , is given by

$$A = \frac{|R/2|}{\ln \frac{e^{|R|} - e^{-|R/2|}}{e^{|R/2|} - 1}} \quad (10)$$

This choice of  $A$ , together with the subsequent piece-wise linear amplifier  $z$ , yields an approximation that is exact for very small and for very large values of  $x$  and also for those  $x$  for which  $Z\{x\} = \pm R/2$ . This second approximation is especially good for large  $R$  ( $R > 16$ ) as can be seen from Fig. 5 where  $\frac{1}{R} Z\{x\}$  is plotted versus  $\frac{Ax}{R}$  for several values of  $R$ .



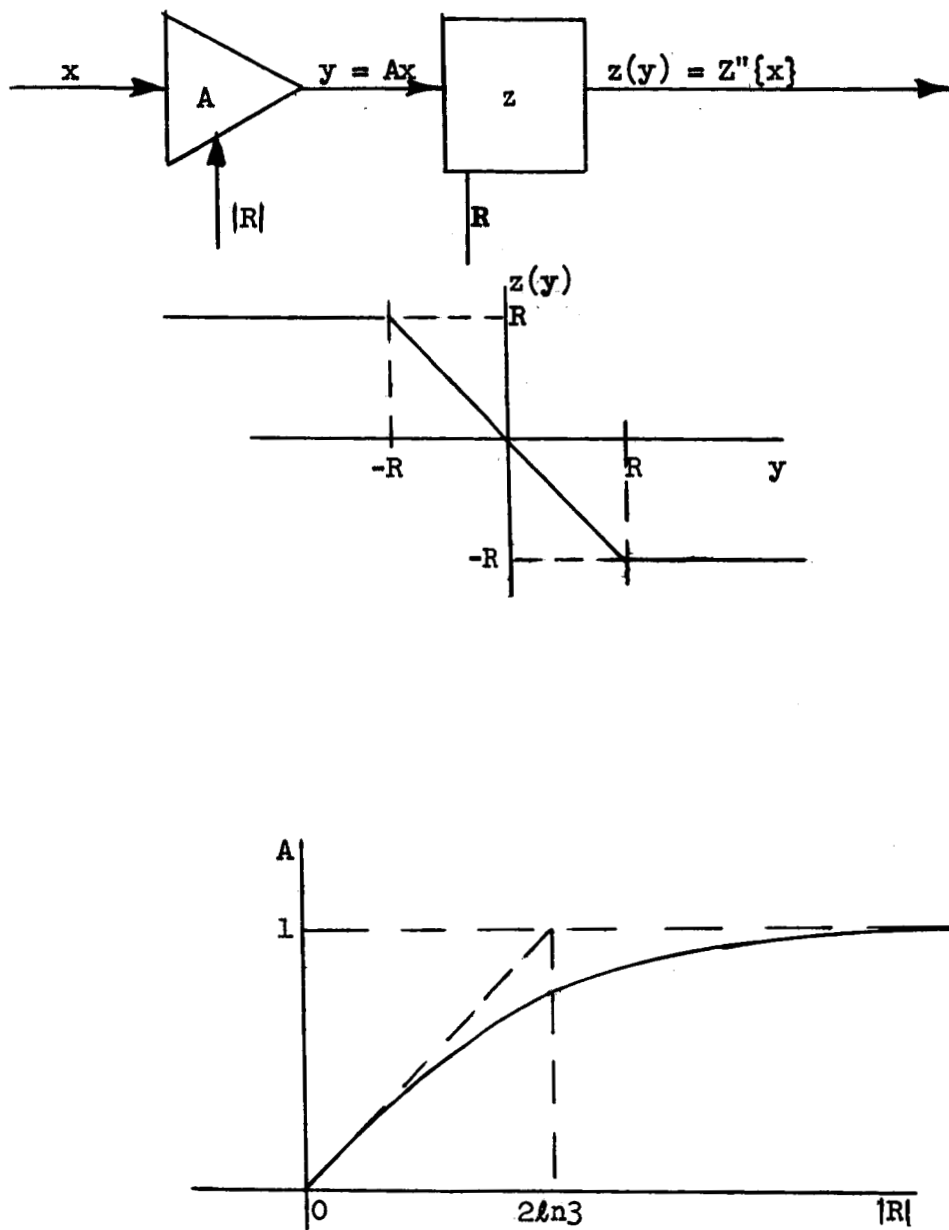


Fig. 4 Second Approximation to  $Z\{x\}$

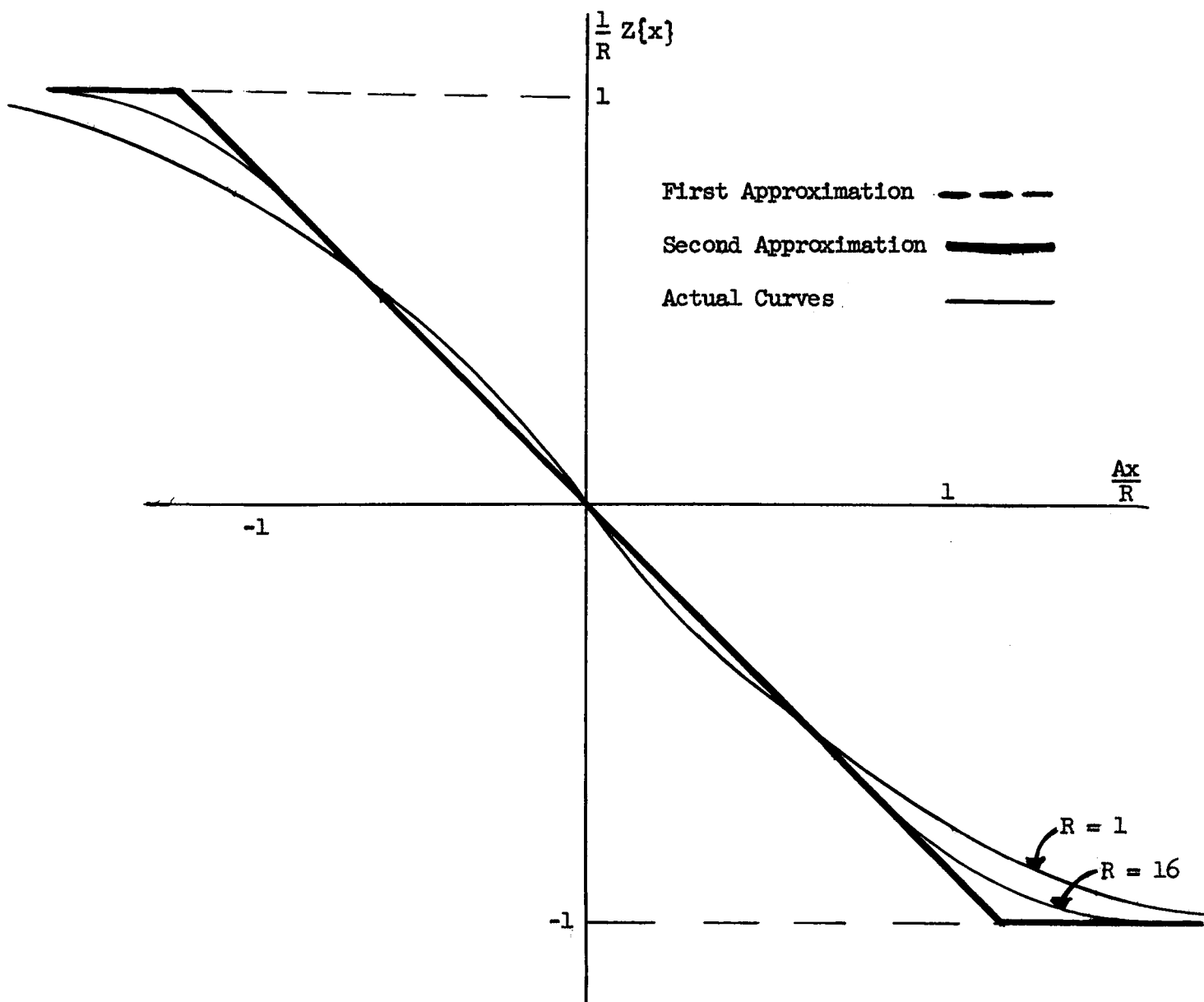


Fig. 5 Comparison of Approximations to  $Z\{x\}$

#### 4. Performance

The non-linearity of the ML decision statistic  $\Lambda_k$ , as given by (3), discourages an exact analytical determination of the per-symbol probability of error  $P_e$ . We will be content, therefore, to find upper and lower bounds for  $P_e$ .

A reasonable lower bound is easily established. If we want to plot  $P_e$  versus  $\rho$ , the signal-to-noise ratio, then we must choose  $r$ , the index of interference, as a parameter. Obviously, the most favorable condition is  $r = 0$  which means that the main portion of the pulse  $s(t)$  is orthogonal to its tail. If such is the case, proper filtering can extract this tail and the particular time slot occupied by the tail is unimportant. We may consider that it is, in fact, sent during the same time slot as the main body of the pulse. Thus the total signal energy is available in one baud and we have the usual, interference-less probability of error given by  $\text{Erfc}\{\sqrt{\rho}\}$ , where

$$\text{Erfc}\{x\} = \frac{1}{\sqrt{2\pi}} \int_x^{\infty} e^{-\frac{t^2}{2}} dt. \quad (11)$$

Our lower bound on  $P_e$  is, then,

$$\text{Erfc}\{\sqrt{\rho}\} < P_e. \quad (12)$$

To establish the upper bound on  $P_e$  we establish the probability of error for a sub-optimum detector. To this end we separate  $A_k$  of Equation (1) into

$$A_k = c_k + d_k, \quad (13)$$

where

$$c_k = \frac{4}{N_0} \int_{kT}^{(k+1)T} y(t) s(t-kT) dt \quad (14)$$

and

$$d_k = \frac{4}{N_0} \int_{(k+1)T}^{(k+2)T} y(t) s(t-kT) dt. \quad (15)$$

Thus  $c_k$  is the correlation of the data with the first part of the pulse,  $s(t)$ , and  $d_k$  is the correlation of the data with the pulse's tail. With these definitions we can write the optimum statistic  $\Lambda_k$  of Equation (3) as

$$\begin{aligned} \Lambda_k = & c_k + Z\{c_{k-1} + d_{k-1} + Z\{c_{k-2} + d_{k-2} + \dots\}\} \\ & + d_k + Z\{d_{k+1} + c_{k+1} + Z\{d_{k+2} + c_{k+2} + \dots\}\}. \end{aligned}$$

Now we use the first approximation  $Z'\{x\}$  to  $Z\{x\}$  as given by Equation (9) to yield a new statistic

$$\begin{aligned} c_k - R \operatorname{Sgn}\{c_{k-1} + d_{k-1} - R \operatorname{Sgn}\{\dots\}\} \\ + d_k - R \operatorname{Sgn}\{d_{k+1} + c_{k+1} - R \operatorname{Sgn}\{\dots\}\}. \end{aligned}$$

The statistic to be studied,  $U_k$ , is then found by setting to zero all  $d$  terms under the first  $\operatorname{Sgn}$  bracket and all  $c$  terms under the second. Thus

$$U_k = U_k^- + U_k^+, \quad (16)$$

where

$$U_k^- = c_k - R \operatorname{Sgn}\{U_{k-1}^-\} \quad (17)$$

and

$$U_k^+ = d_k - R \operatorname{Sgn}\{U_{k+1}^+\}. \quad (18)$$

Note that  $U_k^-$  is a "tail cancellation" detector\* operating only on the data up to  $(k+1)T$  and  $U_k^+$  is its counterpart operating only on data after  $(k+1)T$ .

It can be shown\*\* that if  $U_k^-$  is used as a decision statistic for  $\mu_k$  it yields a probability of error  $P_e^-$  given by

$$P_e^- = \frac{\text{Erfc}\left\{\sqrt{\frac{C}{2}}\right\}}{1 + \text{Erfc}\left\{\sqrt{\frac{C}{2}}\right\} - \frac{1}{2} \text{Erfc}\left\{\frac{C+2R}{\sqrt{2C}}\right\} - \frac{1}{2} \text{Erfc}\left\{\frac{C-2R}{\sqrt{2C}}\right\}}, \quad (19)$$

where

$$C \equiv \frac{4}{N_0} \int_0^T s^2(t) dt. \quad (20)$$

Thus, we deduce that  $U_k^+$  yields a probability of error

$$P_e^+ = \frac{\text{Erfc}\left\{\sqrt{\frac{D}{2}}\right\}}{1 + \text{Erfc}\left\{\sqrt{\frac{D}{2}}\right\} - \frac{1}{2} \text{Erfc}\left\{\frac{D+2R}{\sqrt{2D}}\right\} - \frac{1}{2} \text{Erfc}\left\{\frac{D-2R}{\sqrt{2D}}\right\}}, \quad (21)$$

where

$$D \equiv \frac{4}{N_0} \int_T^{2T} s^2(t) dt. \quad (22)$$

---

\* $U_k^-$  is exactly the switched mode detector of Reference (6).

\*\*R. A. Gonsalves, unpublished notes for Course 3.906, Northeastern University, 1966; this may also be deduced from Reference (6).

With these definitions of C and D we can write  $U_k$  more explicitly as

$$U_k = \mu_k(C+D) + n_k + R(\mu_{k-1} + \mu_{k+1}) - R\{\text{Sgn } U_{k-1}^-\} - R\{\text{Sgn } U_{k+1}^+\}, \quad (23)$$

where

$$n_k = \frac{4}{N_0} \int_{kT}^{(k+2)T} n(t) s(t-kT) dt. \quad (24)$$

The desired probability of error  $P_e^{+-}$  is

$$P_e^{+-} = P(U_k < 0 | \mu_k = 1)$$

or

$$P_e^{+-} = \frac{1}{4} [P_1 + P_2 + P_3 + P_4], \quad (25)$$

where

$$P_1 = P(U_k < 0 | \mu_{k-1} = 1, \mu_k = 1, \mu_{k+1} = 1), \quad (26)$$

$$P_2 = P(\mu_k < 0 | \mu_{k-1} = 1, \mu_k = 1, \mu_{k+1} = -1),$$

etc. We can evaluate these 4 probabilities, as the following evaluation of  $P_1$  indicates.

From (23) and (26)

$$P_1 = P(C + D + n_k + 2R - R \text{Sgn}\{U_{k-1}^-\} - R \text{Sgn}\{U_{k+1}^+\} < 0 | \mu_{k-1} = 1, \mu_k = 1, \mu_{k+1} = 1). \quad (27)$$

But  $n_k$  is independent of both  $U_{k-1}^-$  and  $U_{k+1}^+$  since, from (24),  $n_k$  depends on the white noise from  $kT$  to  $(k+2)T$  while  $U_{k-1}^-$  considers data prior to  $kT$  and  $U_{k+1}^+$  considers data after  $(k+2)T$ . Also,  $U_{k-1}^-$  and  $U_{k+1}^+$ , conditioned on  $\mu_{k-1} = 1$ ,  $\mu_k = 1$ , and  $\mu_{k+1} = 1$ , are also independent. Thus  $P_1$  expands into

$$\begin{aligned}
P_1 &= P(n_k < -C - D) P(U_{k-1}^- > 0 | \mu_{k-1} = 1) P(U_{k+1}^+ > 0 | \mu_{k+1} = 1) \\
&+ P(n_k < -C - D - 4R) P(U_{k-1}^- < 0 | \mu_{k-1} = 1) P(U_{k+1}^+ < 0 | \mu_{k+1} = 1) \\
&+ P(n_k < -C - D - 2R) P(U_{k-1}^- < 0 | \mu_{k-1} = 1) P(U_{k+1}^+ > 0 | \mu_{k+1} = 1) \\
&+ P(n_k < -C - D - 2R) P(U_{k-1}^- > 0 | \mu_{k-1} = 1) P(U_{k+1}^+ < 0 | \mu_{k+1} = 1) \\
&= Q_e^+ Q_e^- \operatorname{Erfc} \left\{ \sqrt{\frac{C+D}{2}} \right\} + P_e^+ P_e^- \operatorname{Erfc} \left\{ \frac{C+D+4R}{\sqrt{2(C+D)}} \right\} \\
&+ (Q_e^- P_e^+ + Q_e^+ P_e^-) \operatorname{Erfc} \left\{ \frac{C+D+2R}{\sqrt{2(C+D)}} \right\},
\end{aligned}$$

where

$$Q_e^+ = 1 - P_e^+,$$

$$Q_e^- = 1 - P_e^-,$$

since, from (24)  $n_k$  is Gaussian with mean zero and variance  $2(C+D)$ , and since  $P(U_{k-1}^- > 0 | \mu_{k-1} = 1)$  is exactly  $Q_e^- = 1 - P_e^-$ , etc.

In a similar fashion we can establish  $P_2$ ,  $P_3$  and  $P_4$ . The resulting  $P_e^{+-}$  is

$$\begin{aligned}
P_e^{+-} &= (Q_e^- Q_e^+ + \frac{1}{2} P_e^- P_e^+) \operatorname{Erfc} \left\{ \sqrt{\frac{C+D}{2}} \right\} \\
&+ \frac{1}{2} (Q_e^- P_e^+ + P_e^- Q_e^+) \left[ \operatorname{Erfc} \left\{ \frac{C+D+2R}{\sqrt{2(C+D)}} \right\} + \operatorname{Erfc} \left\{ \frac{C+D-2R}{\sqrt{2(C+D)}} \right\} \right] \\
&+ \frac{1}{4} (P_e^- P_e^+) \left[ \operatorname{Erfc} \left\{ \frac{C+D+4R}{\sqrt{2(C+D)}} \right\} + \operatorname{Erfc} \left\{ \frac{C+D-4R}{\sqrt{2(C+D)}} \right\} \right].
\end{aligned} \tag{28}$$

This is our upper bound on  $P_e$  for the ML detector. Thus

$$\text{Erfc}\{\sqrt{\rho}\} < P_e < P_e^{+-} . \quad (29)$$

In the derivation of the upper bound we were required to separate the main portion of the pulse from its tail. Thus, in order to plot  $P_e$  vs.  $\rho$ , we need a new parameter which defines the division of energy.

Let

$$a \equiv \frac{D}{C} = \frac{\int_T^{2T} s^2(t) dt}{\int_0^T s^2(t) dt} \quad (30)$$

be the required parameter. Then Figures 6, 7, 8, and 9 for  $a = .25, .50, .75$  and  $1.0$  show this upper bound, Equation (28), versus  $\rho$  for several values of  $r$ .

Since Schwartz's inequality requires

$$\left[ \int_0^T s(t) s(t+T) dt \right]^2 \leq \int_0^T s^2(t) dt \int_0^T s^2(t+T) dt$$

we have the following inequality for  $C$ ,  $D$ , and  $R$

$$R^2 \leq CD.$$

This implies the inequality

$$|r| \leq \frac{\sqrt{a}}{1+a} \quad (31)$$

and accounts for the choices of the parameter  $r$  in Figures 6, 7, 8, and 9. Finally, since  $P_e^{+-}$  is symmetric in  $R$  and since  $C$  and  $D$  can be interchanged, Figures 6 through 9 apply also for  $a = 4, 2, 1.33$  and  $1$  respectively, and for  $r$  or  $-r$ , as indicated.



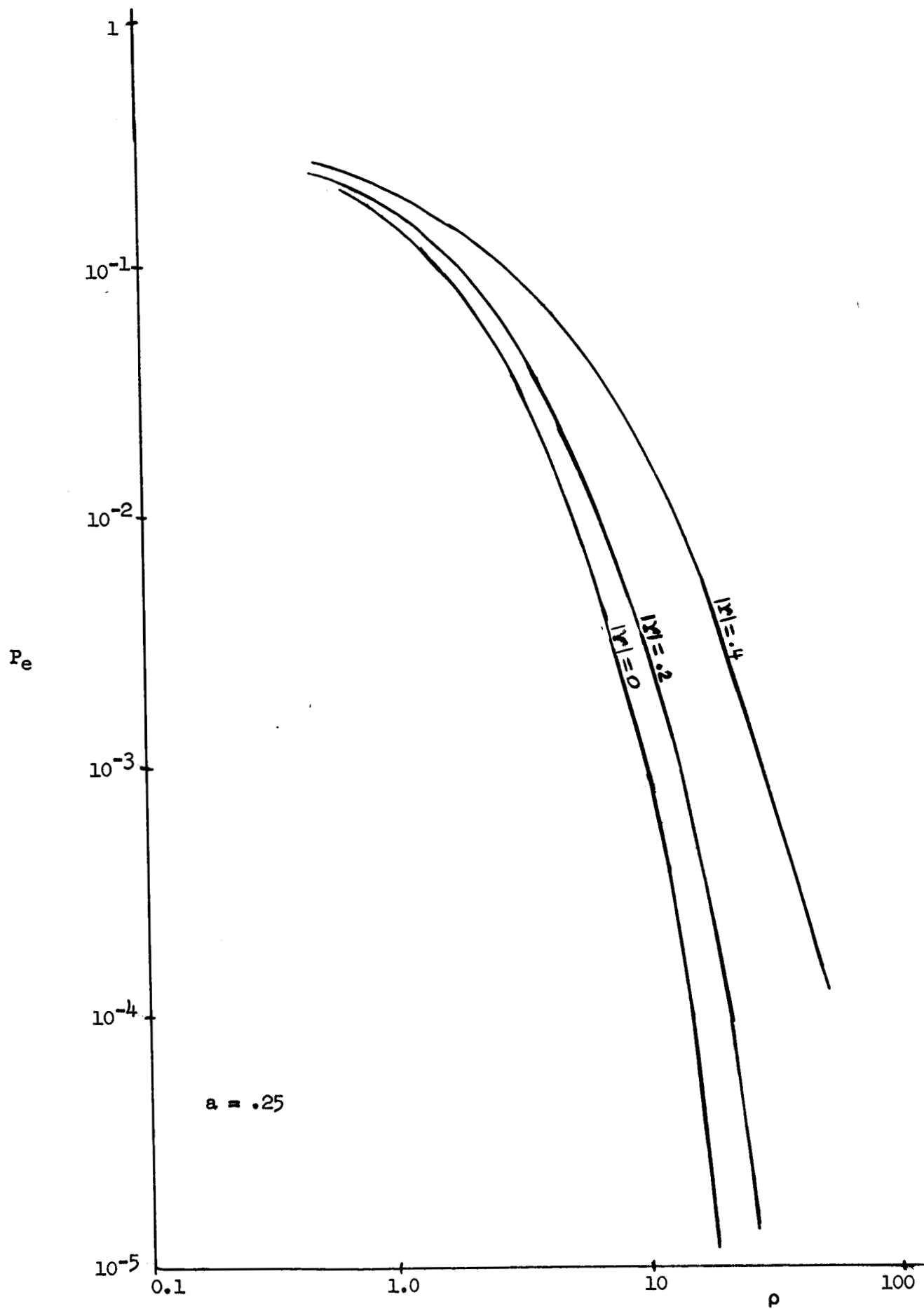


Fig. 6  $P_e$  vs.  $\rho$ ,  $a = .25, 4.0$

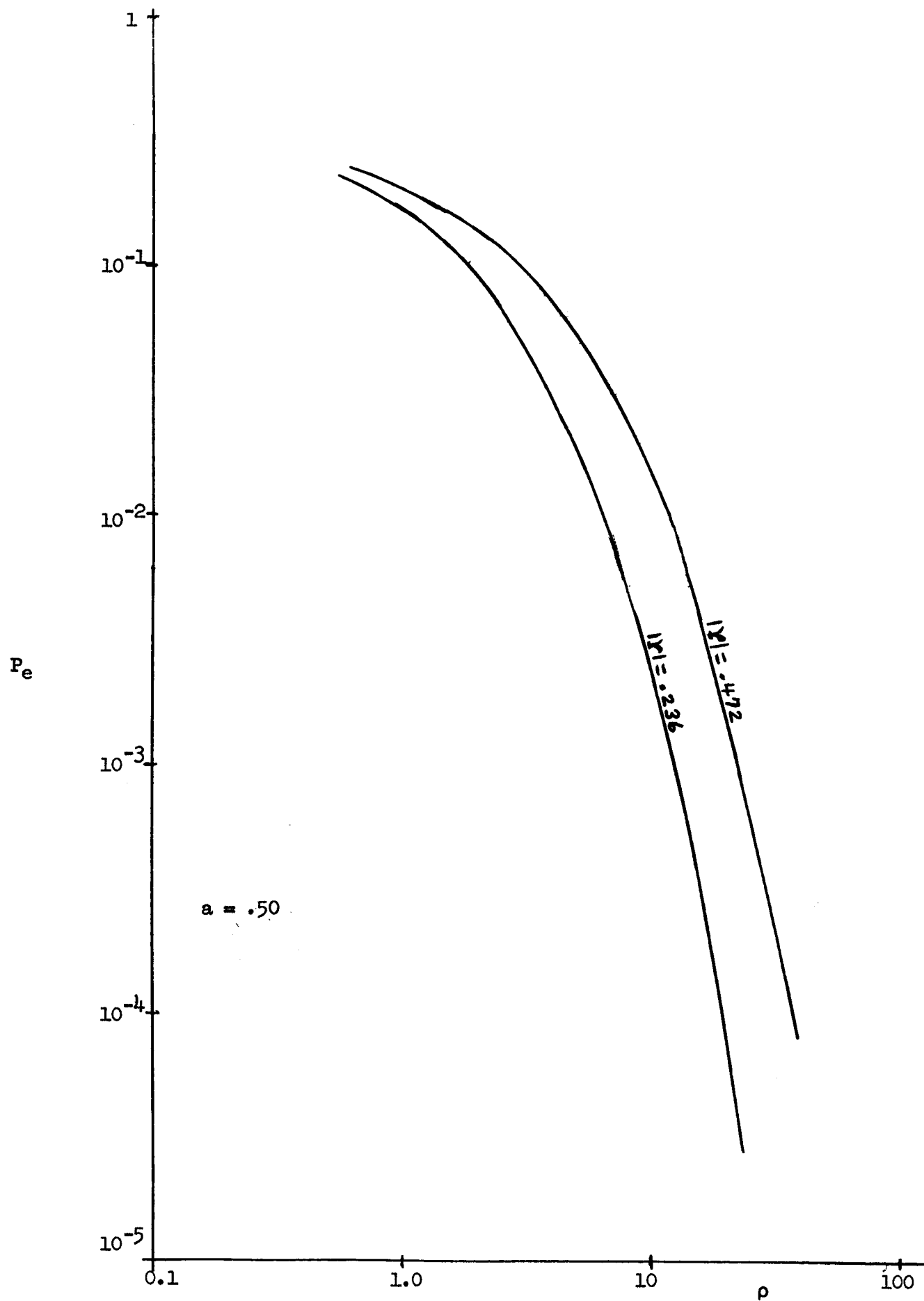


Fig. 7  $P_e$  vs.  $\rho$ ,  $a = .50, 2.0$

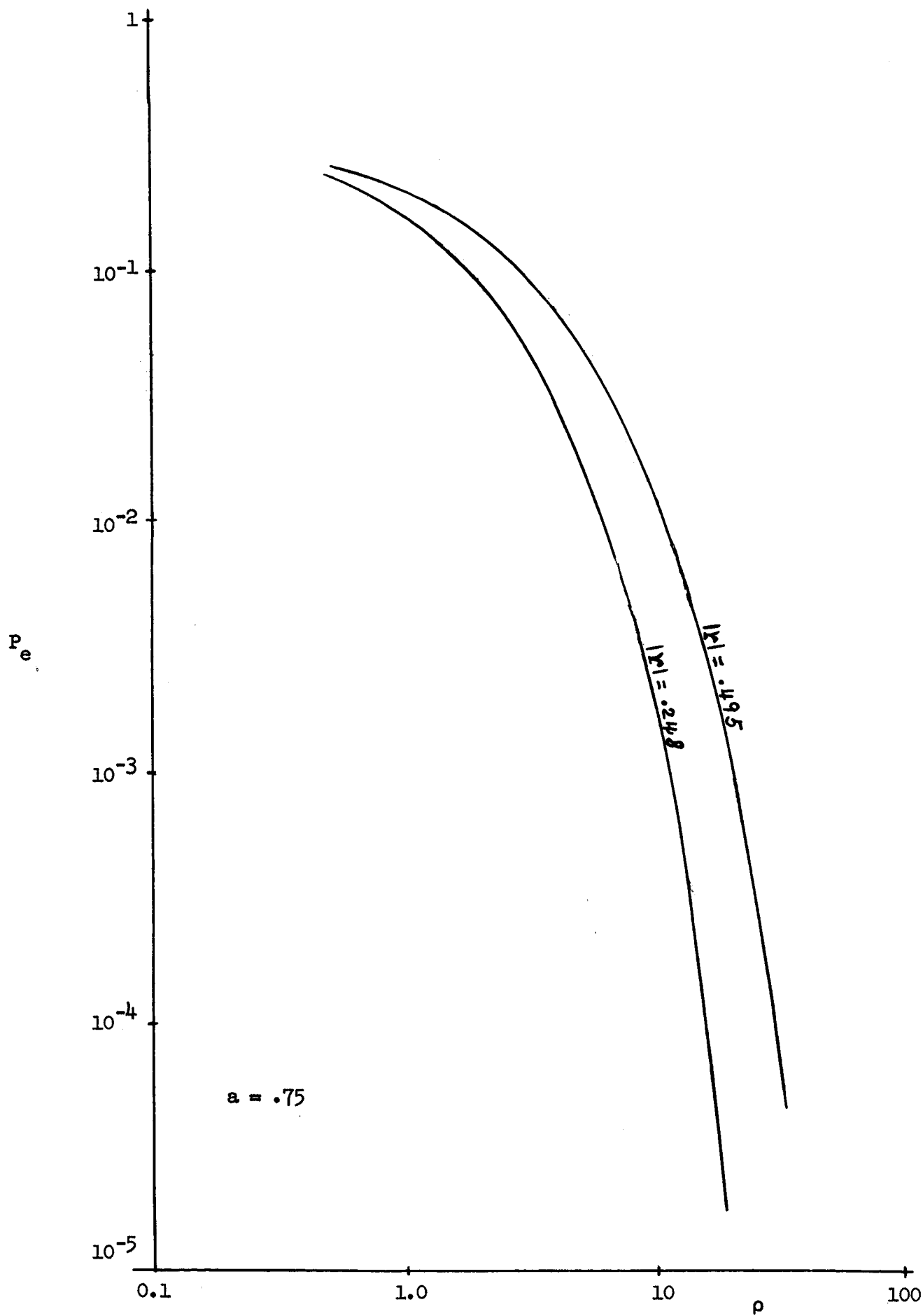


Fig. 8  $P$  vs.  $\rho$ ,  $a = .75$ ,  $1.33$

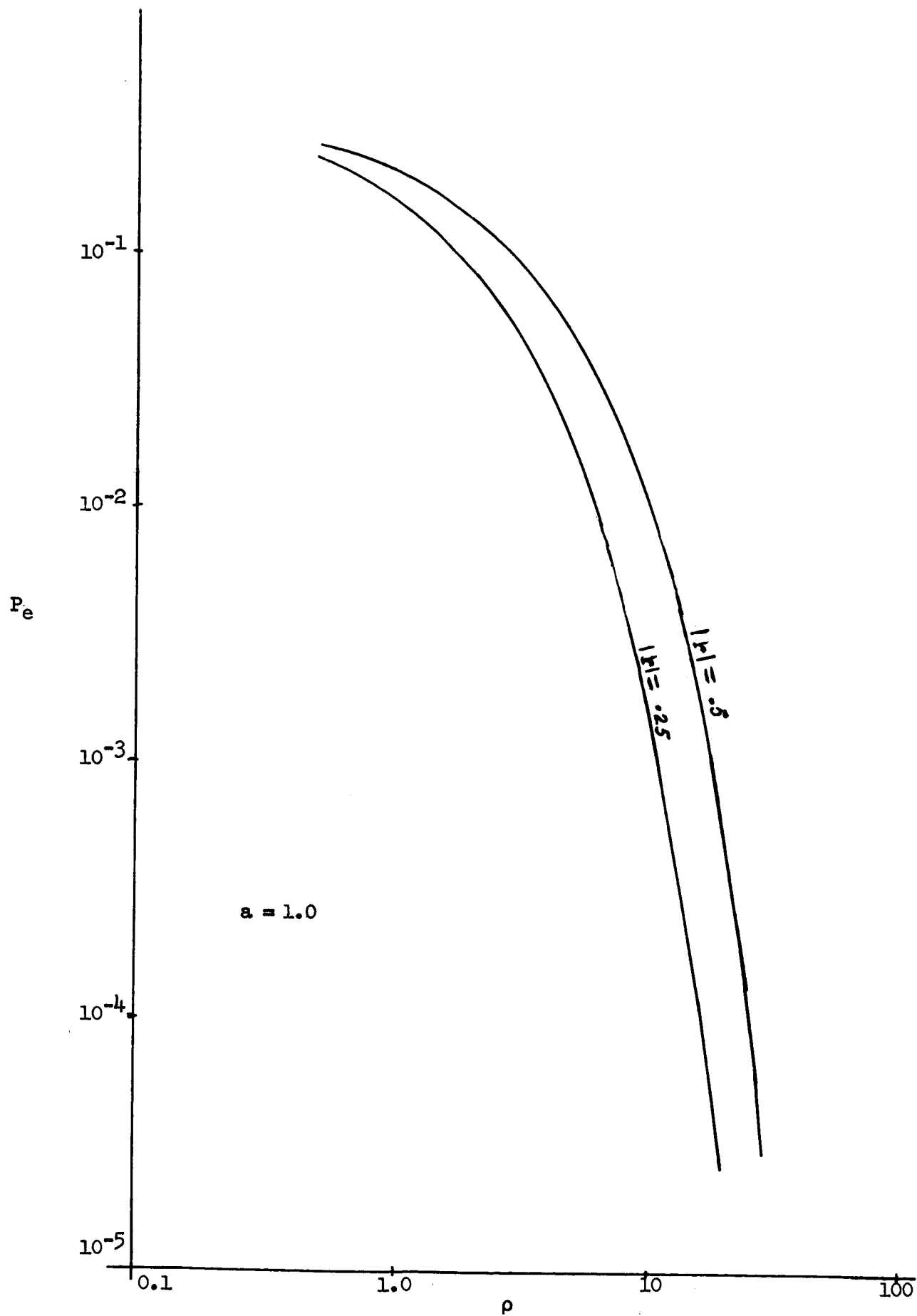


Fig. 9  $P_e$  vs.  $\rho$ ,  $a = 1.0$

To compare the performance of the ML detector with others we assume the unit energy pulse  $s(t)$  as shown in Fig. 10. Since  $s(t)$  is symmetric about  $t = T$ , we have  $a = 1$ . Then the output, of the matched filter of Fig. 2 would be  $g(t)$  as shown, if  $s(t)$  alone were sent. This is, of course, the autocorrelation function  $\phi_{ss}(t)$  of  $s(t)$  delayed by  $2T$  seconds so the index of interference  $r$  is

$$r \equiv \frac{\int_0^{2T} s(t) s(t+T) dt}{\int_0^T s^2(t) dt} = \frac{g(T)}{g(2T)} = .25.$$

From the inequality (31) this is about one-half the maximum interference that can occur. In Fig. 11 we show the resulting upper and lower bounds on  $P_e$  for the ML detector. Also shown in this figure is the tail cancellation detector which operates only on the past data, with probability of error given by Equation (19).

In Reference [4], Fig. 5, Tufts and Aaron present a similar curve for the probability of error of an optimized linear detector. That curve is drawn for a symmetric pulse  $s(t)$ , implying  $a = 1$ , and for  $r = 0.2$ . It is reproduced in Fig. 11 for comparison. We can see that the upper bound on  $P_e$  and this new curve nearly coincide. Since the upper bound is established by considering a detector which uses the tail cancellation principle for both past and future data, this indicates that such a detector is nearly equivalent to an optimum linear detector.

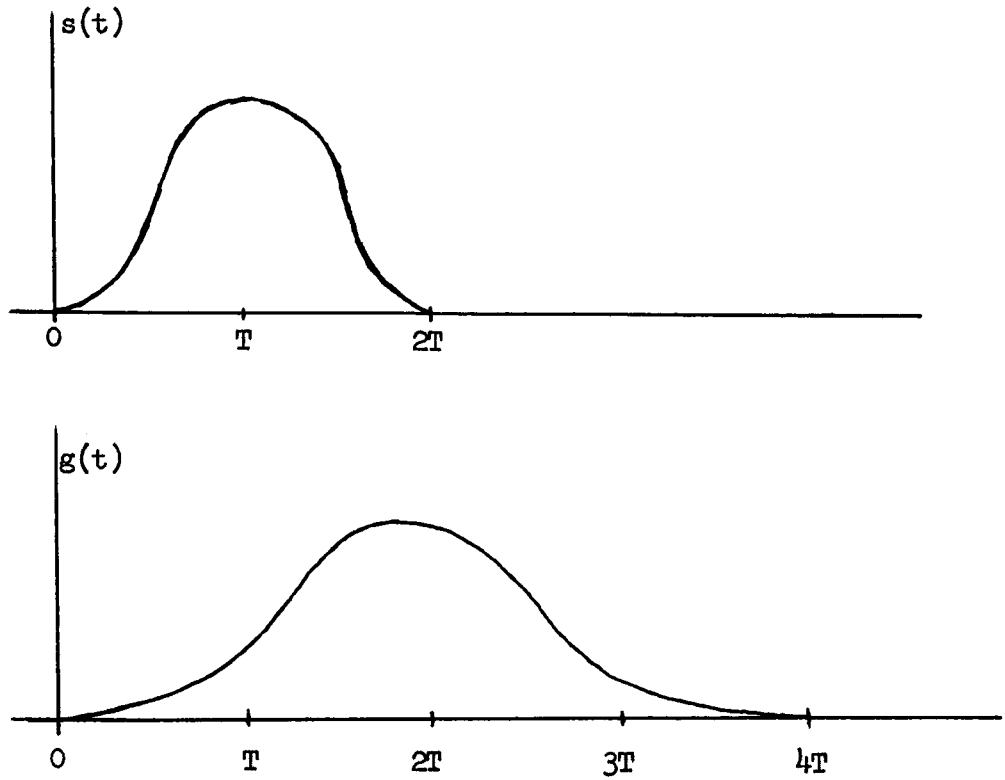


Fig. 10 Input Pulse and the Matched Filter Output

Finally, as discussed in the introduction, the ML detector will always yield a  $P_e$  smaller than that of a linear detector since the ML detector is not restricted by a constraint on linearity. Therefore, the "linear detector" curve of Fig. 11 actually serves as another upper bound on  $P_e$ .

## 5. Extensions

Consider the multi-level case where  $\mu_k$  can take on one of  $M$  distinct values,  $a_1, a_2, \dots, a_M$ . Then using  $a_1$  as a reference, the ML detector computes

$$\Lambda_{ki} = \frac{P(\mu_k = a_i | \text{all data})}{P(\mu_k = a_1 | \text{all data})}, \quad i = 1, 2, \dots, M,$$

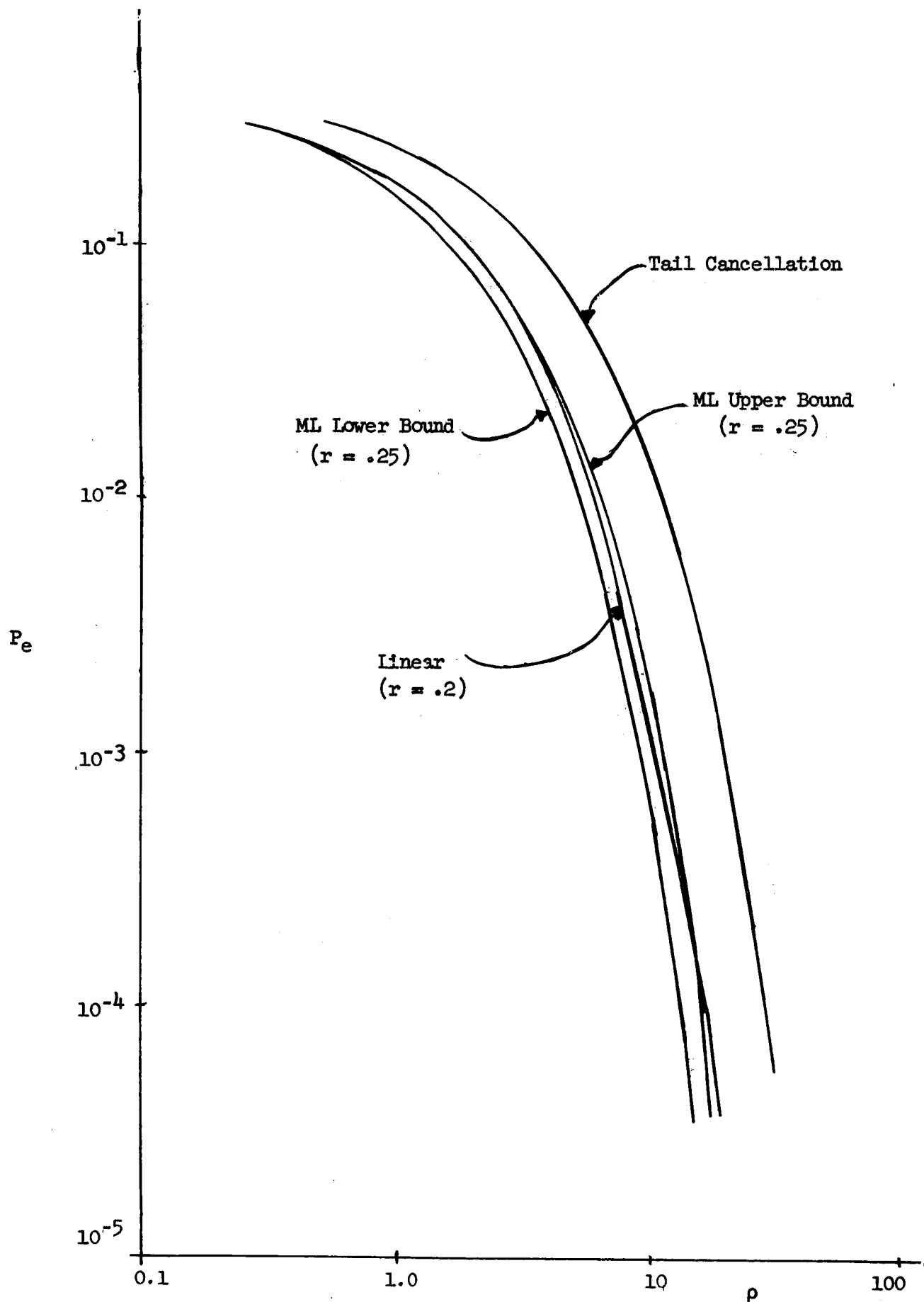


Fig. 11 Comparison of the ML, Tail Cancellation and Linear Receivers

and chooses that  $a_1$  which yields the largest  $\Lambda_{k1}$ . We can show that  $\Lambda_{k1}$  is given by

$$\Lambda_{k1} = (a_1 - a_1) \frac{A_k}{2} + B_1(A_{k-1}, A_{k-2}, \dots) + B_1(A_{k+1}, A_{k+2}, \dots),$$

where  $A_k$  is the same  $A_k$  as that of Equation (1) and the  $B_1$  functions are similar to the previously encountered Z function, Equation (4). It appears that one could find an upper bound on the performance of this detector by a direct extension of the approach used in the binary case. A search for efficient implementation of this detector and the actual bounding of the  $P_e$  are recommended for further study.

The major limitation of the approach taken in this report is the assumption that intersymbol interference exists only between adjacent symbols. It is apparent that this restriction is met if the autocorrelation function  $\phi_{ss}(\tau)$  of  $s(t)$  is zero for  $\tau = \pm 2T, \pm 3T, \dots$ . If such is the case, the signal can actually last for more than two bauds. The time function of Fig. 12 is an example of such an acceptable  $s(t)$ . In fact, we may interpret the restriction to mean that the autocorrelation function is non-zero only at  $\tau = 0$  and at  $\tau = \pm KT$ , K an integer. Such might be the case when the interference is due to multipath, but only two paths are important. See Fig. 13. In implementing such a receiver the delay line tap spacings are simply changed from T seconds to KT seconds.

Finally we recommend for further study the form of the ML detector when the autocorrelation function is non zero at more than one integer multiple removed from  $\tau = 0$ . From the extension above, we hypothesize



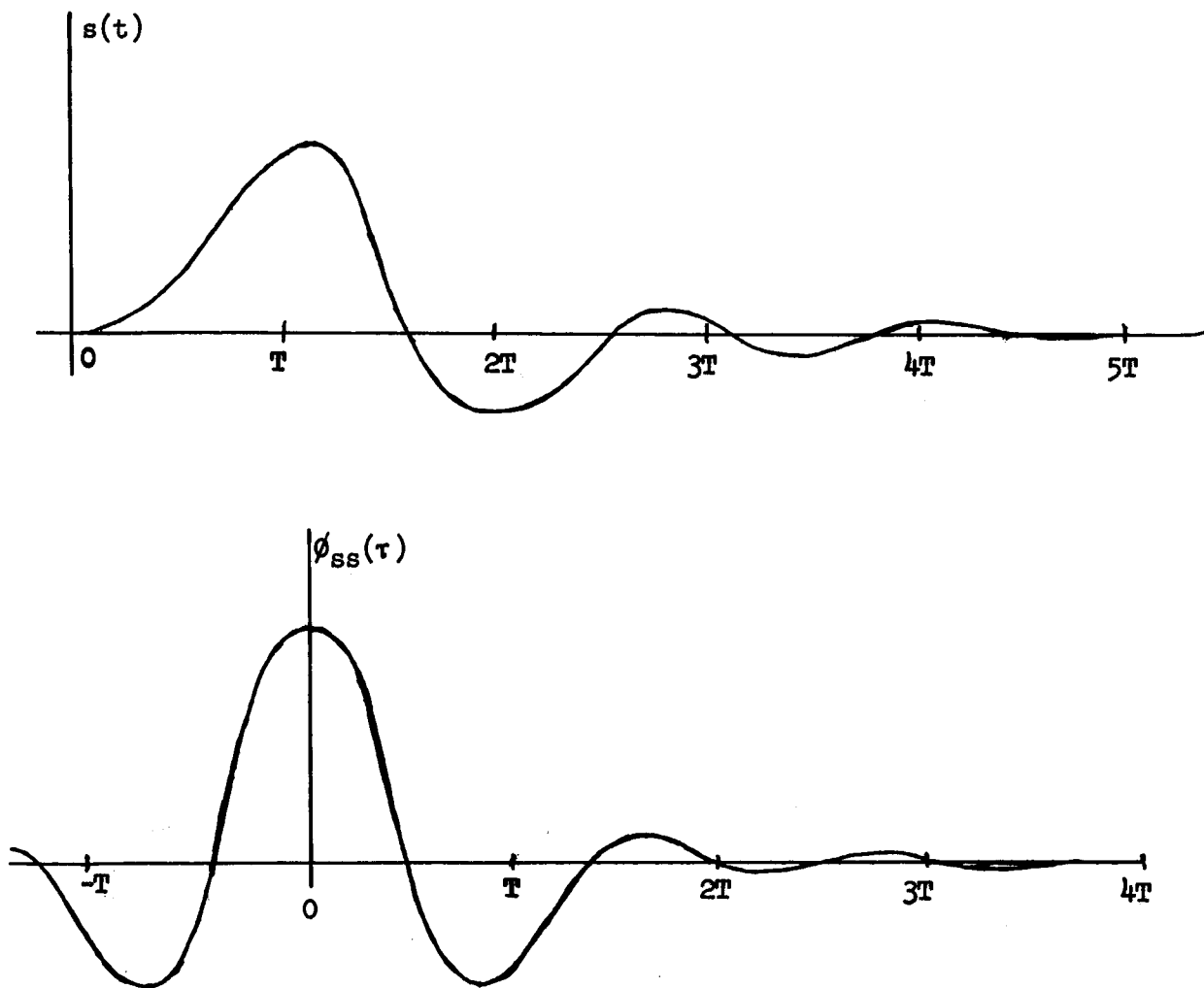


Fig. 12 Acceptable  $s(t)$

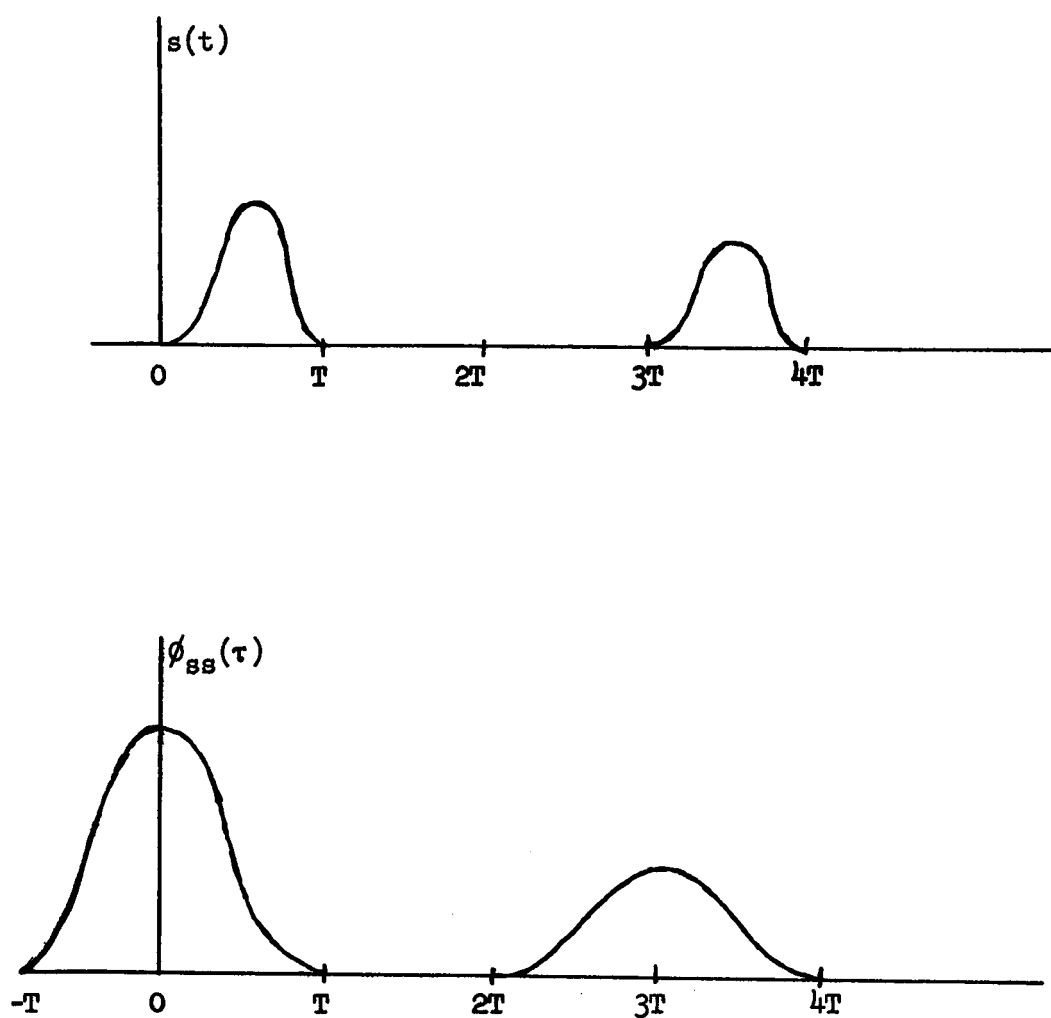


Fig. 13 Another Acceptable  $s(t)$

that a good approximation to this detector, for interference between three symbols, will take the form of Fig. 14, where

$$Z_1\{x\} \equiv \frac{e^x + e^{R_1}}{1 + e^{x+R_1}}, \quad (32)$$

and

$$R_1 \equiv \frac{4}{N_0} \int_{-\infty}^{\infty} s(t) s(t+iT) dt. \quad (33)$$

This detector structure is specified by three parameters,  $R_1$ ,  $R_2$  and  $R_3$ , and using the approximation  $Z_1\{x\} = -R_1 \text{Sgn}\{x\}$  might be easily implemented and analyzed. In that figure

$$\Lambda_k = A_k + B_{k-1}^- + B_{k+1}^+$$

where

$$B_k^- = A_k + Z_1\{B_{k-1}^-\} + Z_2\{B_{k-2}^-\} + \dots$$

and

$$B_k^+ = A_k + Z_1\{B_{k+1}^+\} + Z_2\{B_{k+2}^+\} + \dots$$

## 6. Conclusions

Implementation of the ML detector when intersymbol interference exists only between adjacent symbols is fairly simple. The detector consists of a filter matched to the signal pulse  $s(t)$  followed by a tapped delay line and a feedback loop (Fig. 2). The detector structure, excluding the matched filter, is dependent on a single parameter  $R$ , given by  $R = 2\rho r$ , where  $\rho$  is the signal-to-noise ratio, Equation (7), and  $r$  is the index of interference, Equation (8). Thus the optimum detector structure can easily be adapted to a changing signal-to-noise ratio.

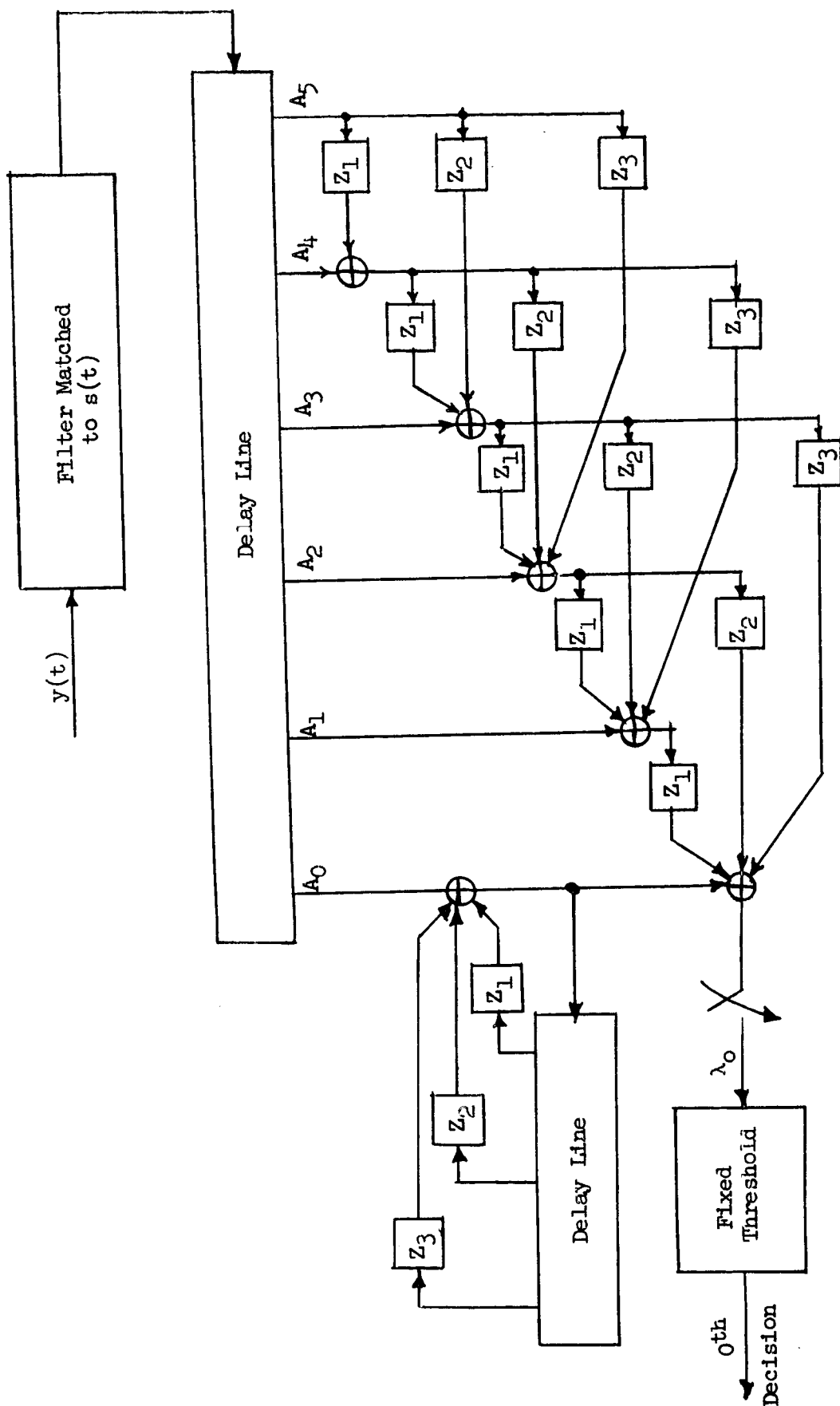


Fig. 14 Possible Detector Configuration for Extended ISI

The performance of the ML detector can be adequately bounded. These bounds are presented in Figures 6 through 9. A gross approximation to the ML detector, that which approximates  $Z\{x\}$  the non-linear amplifier of Equation (4), by a saturating amplifier, as indicated in Equation (9), appears to perform as well as an optimum linear detector and may be easier to implement.

We indicate that these results can be extended to the multi-level case and suggest an approximation to the ML detector for significant interference between more than one symbol.

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13. ABSTRACT It is shown that the maximum-likelihood (ML) detector for noisy, binary channel with restricted intersymbol interference (ISI) consists of a matched filter followed by a tapped delay line. The useful output is a nonlinear function of the tap outputs. Bounds on the per-symbol probability of error indicate that a gross approximation to the ML detector performs as well as an optimum linear detector. The major assumptions are (1) bi-polar binary signals, (2) ISI only between adjacent bauds, (3) stationary additive white, Gaussian noise, and (4) perfect synchronization. Extensions are suggested to remove assumptions (1) and (2) and to handle stationary, non-white Gaussian noise.		

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